

## Hello

About me

A keen railwayman for 10 years

I've operated on both the KWVR and the mainline railway network for the past 5 years.

Became a fireman at age 19

Completed my final year at Huddersfield University and attained a degree in Mechanical Engineering, my dissertation being this subject talked about today.

Carrying on this year and next to hopefully attain a Masters qualification.


## Introduction

War Department locomotive number 79257 was built at Vulcan Foundry Newton Le- Willows Preston in January 1945. Constructed to aid the war effort.


History








## Procedure

## Step 1 <br> Create a CAD model of the locomotive frame on <br> Solidworks

## Step 4

Identify areas of high stress and attain displacement

## Step 2 <br> Calculate forces to be applied onto horn guides <br> within frame

Step 5

Create modifications and add to the frame to reduce the stress application

## Step 3

Mesh and apply forces to frame

## Step 6

Simulate, ascertain whether modifications have strengthened frame.

## The Plan - Step 1

Using $21^{\text {st }}$ century technology to improve a product of the mid $20^{\text {th }}$ century.


## Calculation of Forces longitudinal - Step 2

Piston Force $=$ Steam Pressure $x$ Piston Area

$$
\begin{gathered}
225 \times \frac{\pi \times 19^{2}}{4} \\
225 \times 283.53=63794 \\
63794 \mathrm{lbs}=28936.47 \mathrm{~kg} \\
28936.47 \times 9.81=283866.77 \mathrm{~N} \\
283866.77 \times 0.7=198706.739 \mathrm{~N} \\
T_{1}=P\left(D-\frac{S}{D}\right) \\
T_{1}=198706.739\left(1.44-\frac{0.3683}{1.44}\right) \\
T_{1}=235315.6958 \\
\frac{T_{1}}{4}=58828.92
\end{gathered}
$$

225 psi boiler pressure, 19 -inch diameter piston.

## Change from lbs to kg .

Weight to force.
$30 \%$ reduction to account for steam losing energy through steam circuit.

Equation used as shown opposite
$P$ is the piston force, $D$ is wheel diameter and $S$ is the length of piston stroke.

Thrust force divided by 4 as force shared to 4 coupled wheel sets.

## Calculation of Forces lateral- Step 2

Lateral force calculation with cant


## Lateral force calculation without cant

$F_{\text {Total Lateral }}=\frac{M_{\text {Total }} \times v^{2}}{r}$
$F_{\text {Totai Lateral }}=\frac{70000 \times 11.176^{2}}{200}$
$F_{\text {Total Lateral }}=43716 \mathrm{~N}$
$F_{T L} / 4=10929 \mathrm{~N}$
$2 F_{L}=10929 / 2=5464 \mathrm{~N}$
$F_{L}=5464 / 2=2732 \mathrm{~N}$

- $\quad \mathrm{M}$ Total is the total weight of the locomotive in kg.
- $\quad \mathrm{V}^{\wedge} 2=$ the cornering speed in $\mathrm{m} / \mathrm{s}$
- $r=$ The radius of the corner in $m$
- The total force is divided by 4 across all driving axles.
- This then divided by 2 over each wheel
- Finally, the amount is divided again by two for application onto each of the 4-horn guide axlebox side contact faces.


Fla. 2.
Axlebox Forces Outside Cylinder Engine. Right Hand Crank Leading.
(Symbols as on Fig. 1)

## Forces on RaH. Axlebox due to:-

1. Static weight.
2. Nearside crank, R.H
3. Farside crank, L.H.
4. Nearside coupling rod, R.H.
5. Farside coupling rod, L.H

6 Tractive force
$\mathrm{PR}=$ Piston thrust - right hand side $\mathrm{PL}=$ Piston thrust - left hand side $\mathrm{W}=$ Static weight $\quad \mathrm{T}=$ Tractive force $\quad \mathrm{F}=$ Flange force

SR= Resistance to motion of other coupled wheels transmitted along Side rods - right hand side

SL = Resistance to motion of other coupled wheels transmitted along Side rods - left hand side

## Application Forces - Step 2

Top View Lateral forces applied
Side view longitudinal and vertical forces applied


To correctly simulate the horn guides, working loads for the relevant forces had to be calculated. These comprised of a longitudinal force from the piston thrusts, a lateral forces for when the loco negotiates track curvature and a vertical static force for the weight of the locomotive.

## Meshing on CAD drawing - Step 3

| Global mesh size | mesh control size | displacement | 1/ mesh control size |
| :---: | :---: | :---: | :---: |
| 4 | 0.8 | 7.1472836 | 1.25 |
|  | 0.7 | 7.1819429 | 1.428571429 |
|  | 0.6 | 7.1387687 | 1.666666667 |
|  | 0.5 | 7.2039609 | 2 |
|  | 0.4 | 7.2377839 | 2.5 |
|  | 0.3 | 7.2857637 | 3.333333333 |
|  | 0.2 | 7.3039393 | 5 |
|  | 0.1 | 7.3006802 | 10 |




Identification of high stress areas - Step 4

von Mises $\mid \mathrm{N} / \mathrm{ma}^{2} \mathrm{~m}_{2}$
$3.8197040 \mathrm{e}+0.08$
$3.5004797 \mathrm{e}+0.08$
$3.1622554 \mathrm{e}+1088$
$2.85401310 \mathrm{e}+068$
$2.5450066 \mathrm{e}+6.6 \mathrm{t}$
$2.2275922 \mathrm{e}+0 \mathrm{DE}$
$19093579 \mathrm{e}+\mathrm{D} 08$
$15911336 e+068$
$12729093 \mathrm{e}=0.01$
$9.5459436 \mathrm{e}+017$
$6.3645050 \mathrm{e}+\mathrm{D07}$
$3.1023624 \mathrm{e}+007$
$11902477 e+003$
$\rightarrow$ Yield strength: $3.7000000 e+008$

## Identification of high displacement- Step 4



Identification of high stress areas with cant applied to track - Step 4


Without cant
With cant


## Create frame modifications - step 5

Fourth modification- enlarged top keep


Create frame modifications - step 5
Fifth modification, reduced material on top keep


## Create frame modifications - step 5

Final design


## Have modifications strengthened the frame? - Step 6

| Modification number | With Cant |  | Without Cant |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Stress $\mathrm{N} / \mathrm{m}^{\wedge} 2\left(\times 10^{\wedge} 8\right)$ | Displacement $(\mathrm{mm})$ | Stress N/m^2 ( $\left.\times 10^{\wedge} 8\right)$ | Displacement (mm) |
| Current design | 3.631 | 3.457 | 3.885 | 4.397 |
| 1 | 3.878 | 1.278 | 3.650 | 1.566 |
| 2 | 3.174 | 1.237 | 3.278 | 1.522 |
| 3 | $\mathrm{~N} / \mathrm{A}$ | $\mathrm{N} / \mathrm{A}$ | 4.003 | 1.257 |
| 4 | 2.849 | 1.191 | 2.829 | 1.455 |
| 5 | 2.914 | 1.192 | 2.910 | 1.457 |
| 6 | 2.482 | 1.191 | 2.677 | 1.384 |

## Have modifications strengthened the frame? - Step 6

| Modification number | With Cant |  | Without Cant |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Stress $\mathrm{N} / \mathrm{m}^{\wedge} 2\left(\times 10^{\wedge} 8\right)$ | Displacement (mm) | Stress $\mathrm{N} / \mathrm{m}^{\wedge} 2\left(\times 10^{\wedge} 8\right)$ | Displacement (mm) |
| Current design | 3.631 | 3.457 | 3.885 | 4.397 |
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\% decrease= 32\% \% decrease= 65.5\% \% decrease= 31\% \% decrease=69 \%

Final Comment





Thank You!


Any Questions?

